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# Using molecular simulations for screening of zeolites for separation of CO<sub>2</sub>/CH<sub>4</sub> mixtures

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#### Abstract

Using Grand Canonical Monte Carlo (GCMC) and molecular dynamics (MD) simulation techniques 12 different zeolites were screened to determine which one would yield the best membrane separation selectivity for separation of  $CO_2$  and  $CH_4$ . The choice of the zeolite has a significant influence on both the sorption and diffusion selectivities. It was found that zeolites CHA and DDR, that have cages separated by narrow windows, yielded the best permeation selectivities.

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# 1. Introduction

The separation of  $CO_2$  from natural gas is an important problem. The natural gas stream is available at high pressures of a few megapascals, and can be considered to be primarily methane (CH<sub>4</sub>).  $CO_2$  is a longer, slender molecule; CH<sub>4</sub> is a more compact molecule with a slightly larger cross-section. Fig. 1 presents cartoons showing approximate molecular dimensions of  $CO_2$ , CH<sub>4</sub> and N<sub>2</sub>; these dimensions were estimated using published force fields for molecule–molecule interactions [1–3]. The subtle differences in the molecular dimensions of the two molecules can be exploited by allowing them to adsorb, and subsequently diffuse, across zeolite membranes [4–6]. From a practical point of view it is advantageous to use a membrane separation process in which CH<sub>4</sub> is retained on the high pressure side and CO<sub>2</sub> permeates selectively across to the membrane. Let us define the permeation selectivity

$$\alpha_{\text{perm}} = \frac{N_1/N_2}{f_1/f_2} \tag{1}$$

In Eq. (1)  $N_1$  and  $N_2$  represent the steady-state fluxes of CO<sub>2</sub>(1) and CH<sub>4</sub>(2) crossing the membrane and  $f_1$  and  $f_2$  are the partial gas phase fugacities of the two species in the upstream compartment of the membrane. The flux of any species is related to its

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chemical potential gradient by the Maxwell–Stefan equations [7]

$$-\rho \frac{q_i}{RT} \nabla \mu_i = \sum_{\substack{j=1\\j \neq i}}^n \frac{q_j N_i - q_i N_j}{q_{j,\text{sat}} \mathcal{D}_{ij}} + \frac{N_i}{\mathcal{D}_i}, \quad i = 1, \dots, n$$
(2)

In Eq. (2)  $D_i$  is the Maxwell–Stefan diffusivity of species *i*,  $q_i$  the molar loading,  $q_{i,sat}$  the saturation capacity of species *i*, and  $D_{ij}$  are the binary exchange coefficients. The gradient of the chemical potentials can be related to the gradients in the loadings by defining a matrix of thermodynamic factors

$$\frac{q_i}{RT}\nabla\mu_i = \sum_{j=1}^n \Gamma_{ij}\nabla q_j, \quad \Gamma_{ij} \equiv \frac{q_i}{f_i}\frac{\partial f_i}{\partial q_j}, \quad i, j = 1, \dots, n$$
(3)

The accurate determination of the saturation capacities  $q_{i,sat}$  is essential in order to estimate the diffusion fluxes in the mixture; these can be obtained from the pure component sorption isotherms provided these are available up to saturation limits.

For *screening* purposes we consider an equimolar gas mixture in the upstream compartment, i.e.  $f_1 = f_2$ , take the downstream loadings to be vanishingly small, and approximate Eq. (4) by

$$\alpha_{\text{perm}} = \frac{D_{1,\text{self}}}{D_{2,\text{self}}} \frac{q_1}{q_2} = \alpha_{\text{diff}} \alpha_{\text{sorp}} \tag{4}$$

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Nomenclature

$\mathbf{D}_i$	Maxwell–Stefan diffusivity of species $i$ (m <sup>2</sup> s <sup>-1</sup> )
$f_i$	fugacity of species <i>i</i> (Pa)
$\langle n_i \rangle$	ensemble average number of molecules in sam-
	pling volume
$N_i$	molar flux of species i across membrane
	$(\text{mol}\text{m}^{-2}\text{s}^{-1})$
$q_i$	molar loading (mol/kg)
$q_{i,sat}$	saturation loading (mol/kg)
R	gas constant (8.314 J mol <sup>-1</sup> K <sup>-1</sup> )
Т	absolute temperature (K)
Greek l	etters
$\alpha_{ m diff}$	diffusion selectivity
$\alpha_{\rm perm}$	permeation selectivity
$\alpha_{\rm sorp}$	sorption selectivity
$\Gamma_{ij}$	thermodynamic factors
$\theta_i$	fractional occupancy of component <i>i</i>
$\mu_i$	molar chemical potential $(J \text{ mol}^{-1})$
ρ	density of zeolite $(\text{kg m}^{-3})$
Subscript	
sat	referring to saturation conditions

where the diffusion selectivity  $\alpha_{\text{diff}}$  is the ratio of the selfdiffusivities of components 1 and 2, i.e.



Fig. 1. Cartoon showing the approximate molecular dimensions of  $\mathrm{CO}_2,\,\mathrm{CH}_4$  and  $\mathrm{N}_2.$ 

and the sorption selectivity  $\alpha_{sorp}$  is defined as the ratio of the molar loadings  $q_i$  of CO<sub>2</sub> and CH<sub>4</sub> at the upstream face of the membrane

$$\alpha_{\rm sorp} = \frac{q_1}{q_2} \tag{6}$$

Recent development in Monte Carlo (MC) and molecular dynamics (MD) simulation techniques, coupled with the availability of high performance computing facilities, have enabled the determination of the adsorption and diffusion characteristics of a variety of molecules in different zeolites with a reasonable degree of accuracy and reliability [8–12]. An earlier study showed the utility of molecular simulations in screening zeolites for separation of hexane isomers [13]. The major objective of the current study is to illustrate the potential of MC and MD simulations in screening zeolites for separation of CH<sub>4</sub> and CO<sub>2</sub> for maximum permeation selectivity. We evaluate various zeolites in with regard to  $\alpha_{sorp}$  and, subsequently,  $\alpha_{diff}$ . We demonstrate that molecular simulations can provide insights into adsorption mechanisms, siting, orientation, and transport of molecules that are not available from experiments alone. Such insights allow the development of more fundamental models for process design.

#### 2. Simulation results and discussion

More than 180 zeolite structures are known [14]. Fig. 2 shows some common topologies. The adsorption isotherms for pure CO<sub>2</sub>, pure CH<sub>4</sub> and equimolar binary mixtures of CO<sub>2</sub> and CH<sub>4</sub> at 300 K in 12 different zeolites were computed using the Grand Canonical Monte Carlo (GCMC) technique. The chosen zeolites fall into three categories consisting of (a) one-dimensional channel structures (AFI, MOR, TON, FER, LTL), (b) intersecting channels (MFI, ISV, BEA), and (c) cages separated by windows (FAU, LTA, CHA, DDR). The simulation methodology, including a description of the force field, is given in Supplementary Data, that includes the complete set of information on the adsorption isotherms, along with snapshots showing the location of the molecules in the various zeolite structures. A selection of the important results is presented and discussed below.

Consider the pure component sorption isotherms of  $CO_2$  and CH<sub>4</sub> in MFI determined experimentally by Zhu et al. [6], Golden and Sircar [15] and Kishima et al. [16]; see Fig. 3a and b. As is conventional, the data are plotted on linear axes. Zhu et al. [6] fitted the data with a single site Langmuir model with saturation capacities of 2.97 and 2.69 mol/kg for CO<sub>2</sub> and CH<sub>4</sub>, respectively. When the same experimental data set is plotted with a logarithmic scale for the pressure axis it becomes apparent that for the range of pressures used in the experiments saturation was not achieved; see Fig. 3c and d. Also plotted in Fig. 3c and d are the GCMC simulation results that can be carried out to pressures say of 10<sup>11</sup> Pa that are not accessible experimentally. The GCMC simulations suggest saturation capacities of 5.8 and 4 mol/kg for CO<sub>2</sub> and CH<sub>4</sub>, respectively. These values correspond to values determined assuming that the pore volume is filled with saturated liquid.



Fig. 2. A selection of zeolite structures. Note that the individual landscapes of zeolites are not all drawn to the same scale.

Fig. 4 shows the experimental data of Himeno et al. [17], indicated by the open symbols, for pure component isotherms of  $CO_2$  and  $CH_4$  in DDR for temperatures of (a) 273 K, (b) 298 K, (c) 323 K, and (d) 348 K. The filled symbols are GCMC simulation results; there is good agreement between the experiments and GCMC simulations confirming the correctness of the force field used in the simulations. On the basis of their experimental data Himeno et al. [17] obtained saturation capacities of approximately 2.8 and 1.7 mol/kg for  $CO_2$  and  $CH_4$ , respectively. The GCMC simulation results appear to indicate that saturation was not achieved in the experiments and the true saturation capacities are significantly higher, about 4.6 and 4.2 mol/kg, for  $CO_2$ and  $CH_4$ , respectively. A further cautionary note is required when fitting of experimental isotherm data for  $CO_2$  and  $CH_4$ . In almost all zeolites these molecules show inflection behavior and therefore a simple single site Langmuir fit is not justified. At least two-site, in most cases three-site Langmuir isotherm fits will be required [18]. This further underlines the problem of determining the saturation capacities from experimental isotherms an isotherm inflection can be mistaken to indicate saturation.

GCMC simulations for the component loadings in equilibrium with an equimolar gas mixture of  $CO_2$  and  $CH_4$  in (a) MFI, (b) CHA, and (c) DDR at 300 K are shown in Fig. 5. With increasing pressure the selectivity increases in favor of  $CO_2$ ; the use of the multicomponent Langmuir model will yield selec-



Fig. 3. Pure component sorption isotherm data for (a and c)  $CO_2$  and (b and d)  $CH_4$  in MFI at 298–305 K. The filled symbols are GCMC simulation results. The open symbols are experimental data of Zhu et al. [6], Golden and Sircar [15] and Kishima et al. [16].

tivities that are independent of the loadings and the pressure. Since the saturation capacities of  $CO_2$  and  $CH_4$  are significantly different from each other, the multicomponent Langmuir model cannot be used to calculate the component loadings for binary mixture sorption because of thermodynamic inconsistencies [19]. The continuous solid lines in Fig. 5 represent calculations of the IAST [20] using three-site Langmuir fits of pure component isotherms as given in an earlier publication [18]. The IAST provides a reasonable accurate estimation of loadings in the mixture and is recommended for use for process design.

The sorption selectivity  $\alpha_{sorp} = q_1/q_2$  was determined from the component loadings for 12 different zeolites, divided into three categories: (a) uni-dimensional channels, (b) intersecting channels, and (c) cages-separated-by-windows; see Fig. 6. In all cases  $\alpha_{sorp} = q_1/q_2$  increases with increasing values of  $q = q_1 + q_2$ . In order to verify that the separation selectivity hierarchy is not influenced by the presence of other species present in natural gas, such as N<sub>2</sub>, simulations were also carried out for a mixture CO<sub>2</sub>/CH<sub>4</sub>/N<sub>2</sub>; the results for  $\alpha_{sorp} = q_1/q_2$  in this ternary mixture are presented in Fig. 7; the results show that the values of  $\alpha_{sorp}$  are practically identical to the ones obtained in the binary mixture. On the basis of the simulation data on  $\alpha_{sorp}$  we can narrow the choice of zeolite to MOR, LTL, MFI, CHA and DDR. We consider each of these zeolites in turn. We note that the  $\alpha_{sorp}$  value for these zeolites are significantly higher than that of MWW, as reported in a recent molecular simulation study [21].

Let us first try to rationalize the  $\alpha_{sorp}$  values observed for MOR at *low* loadings. For this purpose we examine the pure component sorption isotherms; see Fig. 8a. At pressures below about 20 kPa there is practically no adsorption of CH<sub>4</sub> while there is a finite adsorption of CO<sub>2</sub>. The GCMC simulation results are in agreement with the experimental data (open symbols) of Delgado et al. [22] for H-MOR. A snapshot of CO<sub>2</sub> molecules within MOR at 300 K and p = 10 kPa is given in Fig. 8b; this shows that the CO<sub>2</sub> are exclusively located within the side pockets of MOR. Location within side pockets is not very effective during membrane permeation as the molecules cannot diffuse out, except via the main 12-ring channels. In order to confirm this we carried out MD simulations to determine self-diffusivities in an equimolar mixture of CO2 and CH4 in MOR at 300 K. The ratio of the self-diffusivities approximates  $\alpha_{\text{diff}}$  and this data is presented in Fig. 8c. At low loadings the diffusivity of CO<sub>2</sub>



Fig. 4. Pure component sorption isotherm data for  $CO_2$  and  $CH_4$  in DDR at (a) 273 K, (b) 298 K, (c) 323 K, and (d) 348 K. The filled symbols are GCMC simulation results. The open symbols are experimental data of Himeno et al. [17] for DDR.

is about one order of magnitude lower than that of CH<sub>4</sub>; this confirms the idea that at low loadings a vast majority of the CO<sub>2</sub> are trapped in the side pockets. Furthermore, we note that loadings in excess of 2 mol/kg the diffusivities of both species are practically the same. Molecular jumps in uni-dimensional channels are strongly correlated and both species have the same effective mobility; consequently  $\alpha_{diff} \approx 1$ . An analogous picture holds for transport within the uni-dimensional channels of LTL; for this zeolite too the  $\alpha_{diff}$  reach values of unity as the loading is increased above 2 mol/kg; see Fig. 8c. Let us turn to MFI which has an intersecting channels of MFI the molecular jumps of CO<sub>2</sub> and CH<sub>4</sub> are also strongly correlated [3] and therefore the values of  $\alpha_{diff}$ , have values close to unity; cf. Fig. 8c.

The situation with respect to diffusion in CHA and DDR, both having cages separated by narrow windows, is different. Here the inter-cage hops of molecules through the narrow windows separating the two cages occur practically independently of one another because only one molecule can pass through a window at a given time [3]; see snapshots in Fig. 9b and c.  $CO_2$  is a more slender molecule than  $CH_4$ , and the values of  $\alpha_{\text{diff}}$  for CHA and DDR are significantly higher than unity; see Fig. 8c. The window size for DDR is smaller than that of CHA and this is the reason for its higher  $\alpha_{\text{diff}}$ .

The differences in the mixture diffusion characteristics of various zeolite structures are also emphasized in earlier publications [23,24].

Fig. 10 summarizes the data on the permeation selectivity,  $\alpha_{perm}$ , obtained as a product  $\alpha_{sorp}$  and  $\alpha_{diff}$ , as a function of total loading q for MFI, MOR, LTL, CHA and DDR zeolites. We see that the choice of ideal zeolite for use in membrane separations is between CHA and DDR. Also shown by filled symbols in Fig. 10 are experimental permeation selectivities as measured in DDR by van den Bergh et al. [25], and in SAPO-34, an isotype of CHA, by Li et al. [26,27]. The reasonably good agreement between the experimental permeation selectivities and calculations based on molecular simulations bear testimony to the accuracy and applicability of the approach followed in this paper. We also note that the permeation selectivities for CHA and DDR membranes are significantly higher than those obtained from FAU membranes with different Si/Al ratios [28].



Fig. 5. GCMC simulations for the component loadings in equilibrium with an equimolar gas mixture of  $CO_2$  and  $CH_4$  in (a) MFI, (b) CHA, and (c) DDR at 300 K. The continuous solid lines represent calculations of the IAST [20] using three-site Langmuir fits of pure component isotherms; these fit parameters are given in Appendix A1 of the Supplementary Data accompanying this publication.



Fig. 6.  $CO_2/CH_4$  sorption selectivity  $\alpha_{sorp} = q_1/q_2$  as a function of the total mixture loading  $q = q_1 + q_2$ , determined from GCMC binary mixture simulations, determined from GCMC simulations taking  $f_1 = f_2$ , for (a) one-dimensional channel structures (AFI, MOR, TON, FER, LTL), (b) intersecting channels (MFI, ISV, BEA), and (c) cages separated by windows (FAU, LTA, CHA, DDR).



Fig. 7. CO<sub>2</sub>/CH<sub>4</sub> sorption selectivity  $\alpha_{sorp} = q_1/q_2$  as a function of the total mixture loading  $q = q_1 + q_2 + q_3$  in ternary mixture CO<sub>2</sub>/CH<sub>4</sub>/N<sub>2</sub>, determined from GCMC simulations taking  $f_1 = f_2 = f_3$ .



Fig. 8. (a) Pure component isotherm data for CO<sub>2</sub> and CH<sub>4</sub> in MOR at 300 K. Also shown are the experimental data (open symbols) of Delgado et al.[22] for H-MOR. (b) Snapshot of CO<sub>2</sub> in MOR at 300 K and p = 10 kPa. (c) The diffusion selectivity  $\alpha_{\text{diff}}$  for various zeolites, calculated on the basis of MD simulations of self-diffusivities mixtures. The self-diffusivity data in for MFI, MOR and LTL are based on simulations of 1:1 mixtures of CO<sub>2</sub> and CH<sub>4</sub>. For DDR and CHA the presented data are for 3:1 and 10:1 mixtures, respectively, in order to reflect the higher sorption selectivities for the zeolites.



Fig. 9. Snapshots of  $CO_2$  and  $CH_4$  in (a) MFI, (b) CHA, and (c) DDR. These snapshots were made at partial fugacities of 500 and 9500 kPa, respectively for  $CO_2$  and  $CH_4$ . Note that the individual snapshots are not all drawn to the same scale.

The permeation selectivity calculations using  $\alpha_{\text{perm}}$  are good enough for screening purposes. For accurate process design calculations of the fluxes using the M-S equations we need the matrix of thermodynamic factor[ $\Gamma$ ] in Eq. (3). The fluctuation formula of Reed and Ehrlich [29] can be extended to a binary mixture to obtain the following expression for the *inverse* matrix



Fig. 10. The permeation selectivity,  $\alpha_{\text{perm}}$  as a function of total loading q for MFI, MOR, LTL, CHA and DDR zeolites. Also shown by filled symbols are the experimental permeation selectivity data for DDR [25], and SAPO-34 [26,27].

of thermodynamic factors[L]:

$$L_{ji} \equiv \frac{f_i}{q_i} \frac{\partial q_j}{\partial f_i} = \frac{\langle n_i n_j \rangle - \langle n_i \rangle \langle n_j \rangle}{\langle n_i \rangle}$$
(7)

The desired elements of the matrix of thermodynamic factors  $[\Gamma]$  are obtained by matrix inversion:

$$[\Gamma] = [L]^{-1} \tag{8}$$

GCMC simulations using Eq. (8) of  $[\Gamma]$  for CO<sub>2</sub> (1)–CH<sub>4</sub> (2) mixtures in MFI, CHA, and DDR at 300 K are shown in Fig. 11. The continuous solid lines represent calculations of  $[\Gamma]$  with IAST [20] using three-site Langmuir fits of pure component isotherms. It can be concluded that the IAST is of reasonable accuracy in process design calculations of the membrane permeation fluxes.

The procedure outlined above for screening of zeolites for CO<sub>2</sub>/CH<sub>4</sub>, separation can also be applied for separation of CO<sub>2</sub>/N<sub>2</sub>. Fig. 12 shows the CO<sub>2</sub>/N<sub>2</sub> sorption selectivity, $\alpha_{sorp} = q_1/q_3$ , as a function of the total mixture loading  $q = q_1 + q_2 + q_3$  in ternary mixture CO<sub>2</sub>/CH<sub>4</sub>/N<sub>2</sub>, determined from GCMC simulations taking  $f_1 = f_2 = f_3$ . We conclude from this figure that the highest sorption selectivities are obtained with CHA zeolite. MD simulation results for self diffusivities in  $CO_2/N_2$  mixtures in CHA are shown in Fig. 13a. We note that the diffusivity of  $CO_2$  is smaller than that of  $N_2$ . Fig. 13b shows that the calculations of the  $\alpha_{perm}$  for CHA compare reasonably well with the experimental data for Li et al. [26,27] for SAPO-34 membrane; the permeation selectivity values are in the range of 30–35, significantly higher than the values reported by Bernal et al. [30] for MFI membrane. We also note that our study contradicts the conclusions of Jia and Murad [31] who used MD simulations to conclude that the separation selectivity of CHA is lower than that of MFI and FAU.



Fig. 11. GCMC simulations using Eq. (8) of  $[\Gamma]$  for CO<sub>2</sub>(1)–CH<sub>4</sub>(2) mixtures in (a) MFI, (b) CHA, and (c) DDR at 300 K. The continuous solid lines represent calculations of  $[\Gamma]$  with IAST [20] using three-site Langmuir fits of pure component isotherms; these fit parameters are given in Appendix A1 of the Supplementary Data accompanying this publication.



Fig. 12.  $CO_2/N_2$  sorption selectivity $\alpha_{sorp} = q_1/q_3$  as a function of the total mixture loading  $q = q_1 + q_2 + q_3$  in ternary mixture  $CO_2/CH_4/N_2$ , determined from GCMC simulations taking  $f_1 = f_2 = f_3$ .



Fig. 13. (a) The  $CO_2/N_2$  diffusion selectivity  $\alpha_{diff}$  for CHA, calculated on the basis of MD simulations of self-diffusivities mixtures. The presented data are for 20:1 mixtures in order to reflect the higher sorption selectivities for the zeolites. (b) The  $CO_2/N_2$  permeation selectivity,  $\alpha_{perm}$  as a function of total loading *q* for CHA zeolite. Also shown by filled symbols are the experimental permeation selectivity data for SAPO-34 [26,27].

### 3. Conclusions

Twelve different zeolites were screened using GCMC and MD simulation to determine which one would lead to the best permeation selectivity  $\alpha_{perm}$  in a membrane process for separation of CO<sub>2</sub> and CH<sub>4</sub>. On the basis of sorption selectivities  $\alpha_{sorp}$  the choice is narrowed to MOR, LTL, MFI, CHA and DDR. In one-dimensional channel structures (MOR, LTL) and in intersecting channel structures (MFI) there is strong correlation between the molecular jumps and therefore the diffusion selectivity  $\alpha_{\text{diff}}$  is close to unity. High values of  $\alpha_{\text{diff}}$  is achieved by choosing structures in which molecular jumps are uncorrelated; this is the case for zeolites, such as CHA and DDR, that consist of cages separated by narrow windows. CO2 being a longer and slender molecule has a significantly higher diffusivity in such structures. Our study shows that highest  $\alpha_{perm}$  is obtained using CHA and DDR. From a practical point of view other factors such as membrane permeation fluxes would also

need to be considered in the final choice of zeolite membrane. Other considerations that impact on the choice of the zeolite membrane used include Si/Al ratio, membrane thickness, and characteristics of support layer.

Though the emphasis in this paper has been on screening of zeolites, molecular simulation data can also be used for process design and with continued advancement it may be reasonable to expect that processes can be developed and designed entirely *in silico*.

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# Appendix A. Supplementary data

Supplementary data associated with this article can be found, in the online version, at doi:10.1016/j.cej.2007.02.011.

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